

## APPENDIX I.

### COMPUTER PROGRAMS AND SAMPLE RESULTS

As indicated earlier, the equations (45), (48), (50), (53), and (57) represent five independent equations for the determination of the three displacement coefficients,  $a_1$ ,  $a_2$ ,  $a_3$ , the mid-meridian constraining pressure,  $P_c$ , and the wafer centerline deflection,  $\Delta$ . A knowledge of these parameters allows for the determination of the normal and shearing stress distributions from equations (38), (39), (40), and (41), respectively. The applied compressive force can likewise be determined from (43).

If, at a given load, or what is equivalent, a given radius ratio  $R_c/R_o$ , values of  $a_2$  and  $\Delta$  are assumed, then  $a_3$  can be found from equation (50). Using this,  $a_1$  and  $P_c$  are found from (45) and (48), respectively. Equations (53) and (57) are utilized to check the validity of the assumed values of  $a_2$  and  $\Delta$ . A reasonably close approximation can be found for  $\Delta$  by assuming that the wafer maintains its cylindrical shape at all loads. Since the wafer expands more at the mid-meridian plane, the coefficient  $a_2$ , which is a measure of this curvature, will be some initially small negative quantity.

The computer program shown in Figure 21, written in FORTRAN language, starts with an assumed value of -0.010 for  $a_2$ , and then calculates an approximate value of  $\Delta$  from